

# Chapter 2 Rigid Body Motion

## Lecture Notes for A Geometrical Introduction to Robotics and Manipulation

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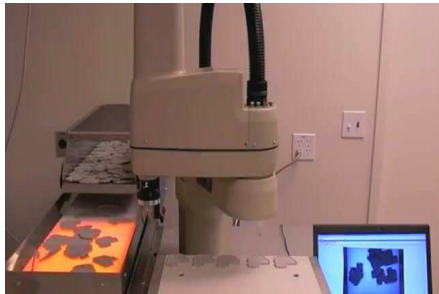
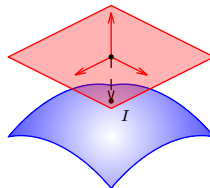
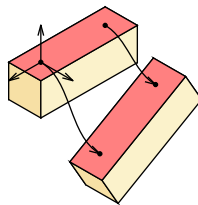
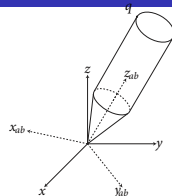
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# Rotational Motion in $\mathbb{R}^3$

- 1 Choose a reference frame  $A$  (spatial frame)
- 2 Attach a frame  $B$  to the body (body frame)

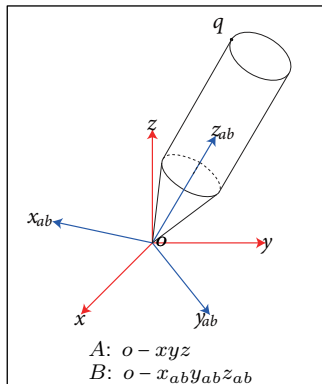


Figure 2.3

$x_{ab} \in \mathbb{R}^3$ : coordinates of  $x_b$  in frame  $A$   
 $R_{ab} = [x_{ab} \ y_{ab} \ z_{ab}] \in \mathbb{R}^{3 \times 3}$ : Rotation (or orientation) matrix of  $B$  w.r.t.  $A$







# Examples of group

- 1  $(\mathbb{R}^3, +)$
- 2  $(\{0, 1\}, + \text{ mod } 2)$
- 3  $(\mathbb{R}, \times)$  Not a group (Why?)
- 4  $(\mathbb{R}_* : \mathbb{R} - \{0\}, \times)$
- 5  $S^1 \triangleq \{z \in \mathbb{C} \mid |z| = 1\}$

**Property 1:**  $SO(3)$  is a group under matrix multiplication.

**Proof :**

- 1 If  $R_1, R_2 \in SO(3)$ , then  $R_1 \cdot R_2 \in SO(3)$ , because
  - $(R_1 R_2)^T (R_1 R_2) = R_2^T (R_1^T R_1) R_2 = R_2^T R_2 = I$
  - $\det(R_1 \cdot R_2) = \det(R_1) \cdot \det(R_2) = 1$
- 2  $e = I_{3 \times 3}$
- 3  $R^T \cdot R = I \Rightarrow R^{-1} = R^T$



# Configuration and rigid transformation

- $R_{ab} = [x_{ab} \ y_{ab} \ z_{ab}] \in SO(3)$   
Configuration Space

- Let  $q_b = \begin{bmatrix} x_b \\ y_b \\ z_b \end{bmatrix} \in \mathbb{R}^3$ : coordinates of  $q$  in  $B$ .

$$q_a = x_{ab} \cdot x_b + y_{ab} \cdot y_b + z_{ab} \cdot z_b$$

$$= [x_{ab} \ y_{ab} \ z_{ab}] \begin{bmatrix} x_b \\ y_b \\ z_b \end{bmatrix} = R_{ab} \cdot q_b$$

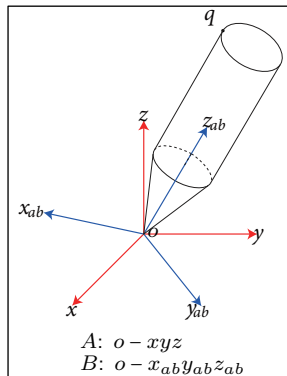


Figure 2.3

- A configuration  $R_{ab} \in SO(3)$  is also a transformation:

$$R_{ab} : \mathbb{R}^3 \rightarrow \mathbb{R}^3, R_{ab}(q_b) = R_{ab} \cdot q_b = q_a$$

A config.  $\Leftrightarrow$  A transformation in  $SO(3)$

**Property 2:**  $R_{ab}$  preserves distance between points and orientation.

$$\textcircled{1} \quad \|R_{ab} \cdot (p_b - q_b)\| = \|p_a - q_a\|$$

$$\textcircled{2} \quad R(v \times \omega) = (Rv) \times R\omega$$

**Proof :**

$$\text{For } a \in \mathbb{R}^3, \text{ let } \hat{a} = \begin{bmatrix} 0 & -a_3 & a_2 \\ a_3 & 0 & -a_1 \\ -a_2 & a_1 & 0 \end{bmatrix}$$

Note that  $\hat{a} \cdot b = a \times b$

$$\begin{aligned} \textcircled{1} \text{ follows from } \|R_{ab}(p_b - p_a)\|^2 &= (R_{ab}(p_b - p_a))^T R_{ab}(p_b - p_a) \\ &= (p_b - p_a)^T R_{ab}^T R_{ab}(p_b - p_a) \\ &= \|p_b - p_a\|^2 \end{aligned}$$

$\textcircled{2}$  follows from  $R\hat{v}R^T = (Rv)^\wedge$  (prove it yourself) □

# Parametrization of $SO(3)$ (the exponential coordinate)

◇ **Review:**  $S^1 = \{z \in \mathbb{C} \mid |z| = 1\}$

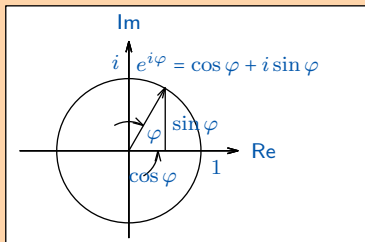


Figure 2.4

## Euler's Formula

“One of the most remarkable, almost astounding, formulas in all of mathematics.”

R. Feynman

◇ **Review:**

$$\begin{cases} \dot{x}(t) = ax(t) \\ x(0) = x_0 \end{cases} \Rightarrow x(t) = e^{at}x_0$$

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$$R \in SO(3), R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}$$

$$r_i \cdot r_j = \begin{cases} 0, & i \neq j \\ 1, & i = j \end{cases} \leftarrow 6 \text{ constraints}$$

$\Rightarrow 3$  independent parameters!

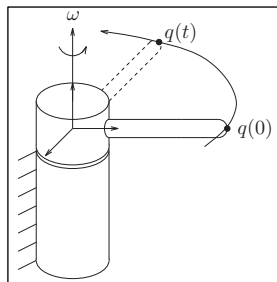


Figure 2.5

Consider motion of a point  $q$  on a rotating link

$$\begin{cases} \dot{q}(t) = \omega \times q(t) = \hat{\omega}q(t) \\ q(0): \text{Initial coordinates} \end{cases}$$

$$\Rightarrow q(t) = e^{\hat{\omega}t} q_0 \text{ where } e^{\hat{\omega}t} = I + \hat{\omega}t + \frac{(\hat{\omega}t)^2}{2!} + \frac{(\hat{\omega}t)^3}{3!} + \dots$$

By the definition of rigid transformation,  $R(\omega, \theta) = e^{\hat{\omega}\theta}$ . Let  $so(3) = \{\hat{\omega} | \omega \in \mathbb{R}^3\}$  or  $so(n) = \{S \in \mathbb{R}^{n \times n} | S^T = -S\}$  where  $\wedge : \mathbb{R}^3 \mapsto so(3) : \omega \mapsto \hat{\omega}$ , we have:

**Property 3:**  $\exp : so(3) \mapsto SO(3), \hat{\omega}\theta \mapsto e^{\hat{\omega}\theta}$

# Rodrigues formula

**Rodrigues' formula** ( $\|\omega\| = 1$ ):

$$e^{\hat{\omega}\theta} = I + \hat{\omega} \sin \theta + \hat{\omega}^2 (1 - \cos \theta)$$

**Proof :**

Let  $a \in \mathbb{R}^3$ , write

$$a = \omega\theta, \omega = \frac{a}{\|a\|} \text{ (or } \|\omega\| = 1), \text{ and } \theta = \|a\|$$

$$e^{\hat{\omega}\theta} = I + \hat{\omega}\theta + \frac{(\hat{\omega}\theta)^2}{2!} + \frac{(\hat{\omega}\theta)^3}{3!} + \dots$$

As

$$\hat{a}^2 = aa^T - \|a\|^2 I, \hat{a}^3 = -\|a\|^2 \hat{a}$$

we have:

$$\begin{aligned} e^{\hat{\omega}\theta} &= I + \left(\theta - \frac{\theta^3}{3!} + \frac{\theta^3}{5!} - \dots\right)\hat{\omega} + \left(\frac{\theta^2}{2!} - \frac{\theta^4}{4!} + \dots\right)\hat{\omega}^2 \\ &= I + \hat{\omega} \sin \theta + \hat{\omega}^2 (1 - \cos \theta) \end{aligned}$$



# Rodrigues formula

**Rodrigues' formula for  $\|\omega\| \neq 1$ :**

$$e^{\hat{\omega}\theta} = I + \frac{\hat{\omega}}{\|\omega\|} \sin \|\omega\|\theta + \frac{\hat{\omega}^2}{\|\omega\|^2} (1 - \cos \|\omega\|\theta)$$

**Proof for Property 3:**

Let  $R \triangleq e^{\hat{\omega}\theta}$ , then:

$$\begin{aligned} (e^{\hat{\omega}\theta})^{-1} &= e^{-\hat{\omega}\theta} = e^{\hat{\omega}^T\theta} = (e^{\hat{\omega}\theta})^T \\ \Rightarrow R^{-1} &= R^T \Rightarrow R^T R = I \Rightarrow \det R = \pm 1 \end{aligned}$$

From  $\det \exp(0) = 1$ , and the continuity of  $\det$  function w.r.t.  $\theta$ , we have  $\det e^{\hat{\omega}\theta} = 1, \forall \theta \in \mathbb{R}$  □

## Property 4: The exponential map is onto.

### Proof :

Given  $R \in SO(3)$ , to show  $\exists \omega \in \mathbb{R}^3, \|\omega\| = 1$  and  $\theta$  s.t.  $R = e^{\hat{\omega}\theta}$

Let

$$R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}$$

and

$$v_\theta = 1 - \cos \theta, c_\theta = \cos \theta, s_\theta = \sin \theta$$

By Rodrigues' formula

$$e^{\hat{\omega}\theta} = \begin{bmatrix} \omega_1^2 v_\theta + c_\theta & \omega_1 \omega_2 v_\theta - \omega_3 s_\theta & \omega_1 \omega_3 v_\theta + \omega_2 s_\theta \\ \omega_1 \omega_2 v_\theta + \omega_3 s_\theta & \omega_2^2 v_\theta + c_\theta & \omega_2 \omega_3 v_\theta - \omega_1 s_\theta \\ \omega_1 \omega_3 v_\theta - \omega_2 s_\theta & \omega_2 \omega_3 v_\theta + \omega_1 s_\theta & \omega_3^2 v_\theta + c_\theta \end{bmatrix}$$

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Taking the trace of both sides,

$$\text{tr}(R) = r_{11} + r_{22} + r_{33} = 1 + 2 \cos \theta = \sum_{i=1}^3 \lambda_i$$

where  $\lambda_i$  is the eigenvalue of  $R, i = 1, 2, 3$

Case 1:  $\text{tr}(R) = 3$  or  $R = I, \theta = 0 \Rightarrow \omega\theta = 0$

Case 2:  $-1 < \text{tr}(R) < 3,$

$$\theta = \arccos \frac{\text{tr}(R) - 1}{2} \Rightarrow \omega = \frac{1}{2s\theta} \begin{bmatrix} r_{32} - r_{23} \\ r_{13} - r_{31} \\ r_{21} - r_{12} \end{bmatrix}$$

Case 3:  $\text{tr}(R) = -1 \Rightarrow \cos \theta = -1 \Rightarrow \theta = \pm\pi$

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Following are 3 possibilities:

$$R = \begin{bmatrix} 1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \end{bmatrix} \Rightarrow \omega = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix},$$

$$R = \begin{bmatrix} -1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & -1 \end{bmatrix} \Rightarrow \omega = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix},$$

$$R = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \Rightarrow \omega = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

Note that if  $\omega\theta$  is a solution, then  $\omega(\theta \pm n\pi), n = 0, \pm 1, \pm 2, \dots$  is also a solution. □

**Definition: Exponential coordinate**

$\omega\theta \in \mathbb{R}^3$ , with  $e^{\hat{\omega}\theta} = R$  is called the exponential coordinates of  $R$

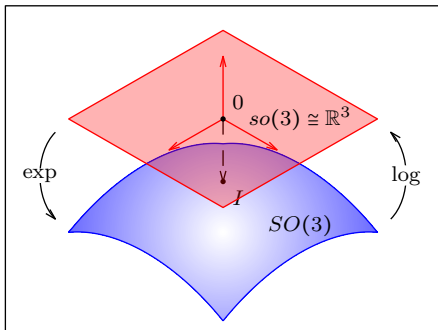


Figure 2.6

**Property 5:**  $\exp$  is 1-1 when restricted to an open ball in  $\mathbb{R}^3$  of radius  $\pi$ .

# Euler's rotation theorem

## Theorem 1 (Euler):

Any orientation is equivalent to a rotation about a fixed axis  $\omega \in \mathbb{R}^3$  through an angle  $\theta \in [-\pi, \pi]$ .

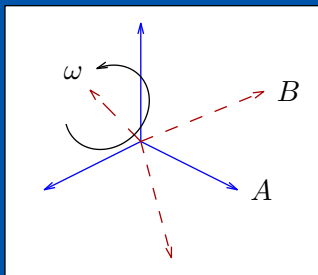


Figure 2.7



1707–1783

$SO(3)$  can be visualized as a solid ball of radius  $\pi$ .

# Other Parametrizations of $SO(3)$

- $XYZ$  fixed angles (or Roll-Pitch-Yaw angle)

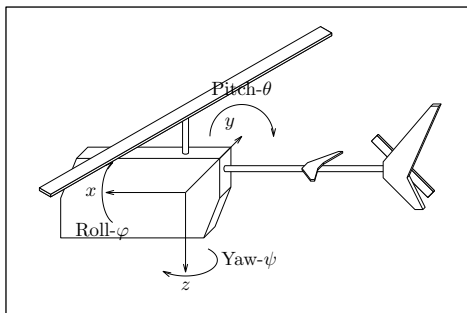


Figure 2.8

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# Other Parametrizations of $SO(3)$

- $XYZ$  fixed angles (or Roll-Pitch-Yaw angle) Continued

$$R_x(\varphi) := e^{\hat{x}\varphi} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \varphi & -\sin \varphi \\ 0 & \sin \varphi & \cos \varphi \end{bmatrix}$$

$$R_y(\theta) := e^{\hat{y}\theta} = \begin{bmatrix} \cos \theta & 0 & \sin \theta \\ 0 & 1 & 0 \\ -\sin \theta & 0 & \cos \theta \end{bmatrix}$$

$$R_z(\psi) := e^{\hat{z}\psi} = \begin{bmatrix} \cos \psi & -\sin \psi & 0 \\ \sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R_{ab} = R_x(\varphi)R_y(\theta)R_z(\psi)$$

$$= \begin{bmatrix} C\theta C\psi & -C\theta S\psi & S\theta \\ S_\varphi S\theta C\psi + C_\varphi S\psi & -S_\varphi S\theta S\psi + C_\varphi C\psi & -S_\varphi C\theta \\ -C_\varphi S\theta C\psi + S_\varphi S\psi & C_\varphi S\theta S\psi + S_\varphi C\psi & C_\varphi C\theta \end{bmatrix}$$

# Other Parametrizations of $SO(3)$

- $ZYX$  Euler angle

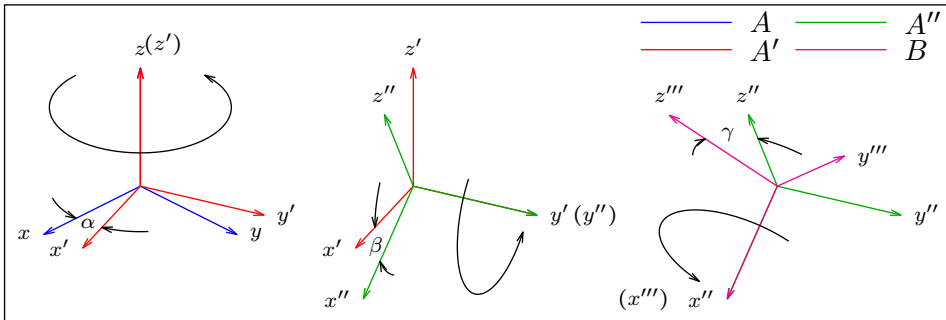


Figure 2.9

$$R_{aa'} = R_z(\alpha)$$

$$R_{a'a''} = R_{y'}(\beta)$$

$$R_{a''b} = R_{x''}(\gamma)$$

$$R_{ab} = R_z(\alpha)R_{y'}(\beta)R_{x''}(\gamma)$$

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# Other Parametrizations of $SO(3)$

- $ZYX$  Euler angle (continued)

$$R_{ab}(\alpha, \beta, \gamma) = \begin{bmatrix} c_\alpha c_\beta & -s_\alpha c_\gamma + c_\alpha s_\beta s_\gamma & s_\alpha s_\gamma + c_\alpha s_\beta c_\gamma \\ s_\alpha c_\beta & c_\alpha c_\gamma + s_\alpha s_\beta s_\gamma & -c_\alpha s_\gamma + s_\alpha s_\beta c_\gamma \\ -s_\beta & c_\beta s_\gamma & c_\beta c_\gamma \end{bmatrix}$$

**Note:** When  $\beta = \frac{\pi}{2}$ ,  $\cos \beta = 0$ ,  $\alpha + \gamma = \text{const} \Rightarrow$  singularity!

$$\beta = \text{atan2}(-r_{31}, \sqrt{r_{32}^2 + r_{33}^2})$$

$$\alpha = \text{atan2}(r_{21}/c_\beta, r_{11}/c_\beta)$$

$$\gamma = \text{atan2}(r_{32}/c_\beta, r_{33}/c_\beta)$$

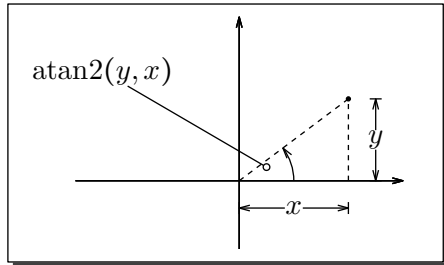


Figure 2.10



# Other Parametrizations of $SO(3)$

## § Quaternions:

$$Q = q_0 + q_1i + q_2j + q_3k$$

$$\text{where } i^2 = j^2 = k^2 = -1, i \cdot j = k, j \cdot k = i, k \cdot i = j$$

**Property 1:** Define  $Q^* = (q_0, q)^* = (q_0, -q)$ ,  $q_0 \in \mathbb{R}, q \in \mathbb{R}^3$

$$\|Q\|^2 = QQ^* = q_0^2 + q_1^2 + q_2^2 + q_3^2$$

**Property 2:**  $Q = (q_0, q), P = (p_0, p)$

$$QP = (q_0p_0 - q \cdot p, q_0p + p_0q + q \times p)$$

**Property 3:** (a) The set of unit quaternions forms a group

(b) If  $R = e^{\hat{\omega}\theta}$ , then  $Q = \left(\cos \frac{\theta}{2}, \omega \sin \frac{\theta}{2}\right)$

(c)  $Q$  acts on  $x \in \mathbb{R}^3$  by  $QXQ^*$ , where  $X = (0, x)$

# Other Parametrizations of $SO(3)$

## □ Unit Quaternions:

Given  $Q = (q_0, q)$ ,  $q_0 \in \mathbb{R}$ ,  $q \in \mathbb{R}^3$ , the vector part of  $QXQ^*$  is given by  $R(Q)x$ , recall that

$$q_0 = \cos \frac{\theta}{2}, q = \omega \sin \frac{\theta}{2}$$

and the Rodrigues' formula:

$$e^{\hat{\omega}\theta} = I + \hat{\omega} \sin \theta + \hat{\omega}^2 (1 - \cos \theta)$$

then

$$R(Q) = I + 2q_0\hat{q} + 2\hat{q}^2$$

$$= \begin{bmatrix} 1 - 2(q_2^2 + q_3^2) & -2q_0q_3 + 2q_1q_2 & 2q_0q_2 + 2q_1q_3 \\ 2q_0q_3 + 2q_1q_2 & 1 - 2(q_1^2 + q_3^2) & -2q_0q_1 + 2q_2q_3 \\ -2q_0q_2 + 2q_1q_3 & 2q_0q_1 + 2q_2q_3 & 1 - 2(q_1^2 + q_2^2) \end{bmatrix}$$

where  $\|Q\| \triangleq q_0^2 + q_1^2 + q_2^2 + q_3^2 = 1$

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# Other Parametrizations of $SO(3)$

## □ Quaternions (continued):

Conversion from Roll-Pitch-Yaw angle to unit quaternions:

$$Q = \left(\cos \frac{\varphi}{2}, x \sin \frac{\varphi}{2}\right) \left(\cos \frac{\theta}{2}, y \sin \frac{\theta}{2}\right) \left(\cos \frac{\psi}{2}, z \sin \frac{\psi}{2}\right) \Rightarrow$$

$$q_0 = \cos \frac{\varphi}{2} \cos \frac{\theta}{2} \cos \frac{\psi}{2} - \sin \frac{\varphi}{2} \sin \frac{\theta}{2} \sin \frac{\psi}{2}$$

$$q = \begin{bmatrix} \cos \frac{\varphi}{2} \sin \frac{\theta}{2} \sin \frac{\psi}{2} + \sin \frac{\varphi}{2} \cos \frac{\theta}{2} \cos \frac{\psi}{2} \\ \cos \frac{\varphi}{2} \sin \frac{\theta}{2} \cos \frac{\psi}{2} - \sin \frac{\varphi}{2} \cos \frac{\theta}{2} \sin \frac{\psi}{2} \\ \cos \frac{\varphi}{2} \cos \frac{\theta}{2} \sin \frac{\psi}{2} + \sin \frac{\varphi}{2} \sin \frac{\theta}{2} \cos \frac{\psi}{2} \end{bmatrix}$$

Conversion from unit quaternions to roll-pitch-yaw angles (?)

† End of Section †

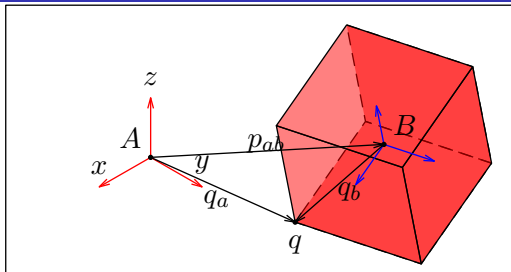
Rigid motion in  $\mathbb{R}^3$ 

Figure 2.11

$p_{ab} \in \mathbb{R}^3$ : Coordinates of the origin of  $B$   
 $R_{ab} \in SO(3)$ : Orientation of  $B$  relative to  $A$

$SE(3) : \left\{ \left[ \begin{array}{cc} R & p \\ 0 & 1 \end{array} \right] \mid p \in \mathbb{R}^3, R \in SO(3) \right\}$ : Orientation of  $B$  relative to  $A$

Or...as a transformation:

$$g_{ab} = (p_{ab}, R_{ab}) : \mathbb{R}^3 \mapsto \mathbb{R}^3$$

$$q_b \mapsto q_a = p_{ab} + R_{ab} \cdot q_b$$

# Homogeneous Representation

Points:

$$q = \begin{bmatrix} q_1 \\ q_2 \\ q_3 \end{bmatrix} \in \mathbb{R}^3$$



$$\bar{q} = \begin{bmatrix} q_1 \\ q_2 \\ q_3 \\ 1 \end{bmatrix} \in \mathbb{R}^4$$

Vectors:

$$v = p - q = \begin{bmatrix} p_1 - q_1 \\ p_2 - q_2 \\ p_3 - q_3 \end{bmatrix} = \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix}$$



$$\bar{v} = \bar{p} - \bar{q} = \begin{bmatrix} p_1 \\ p_2 \\ p_3 \\ 1 \end{bmatrix} - \begin{bmatrix} q_1 \\ q_2 \\ q_3 \\ 1 \end{bmatrix} = \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ 0 \end{bmatrix}$$

- ① Point-Point = Vector
- ② Vector+Point = Point
- ③ Vector+Vector = Vector
- ④ Point+Point: Meaningless

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# Homogeneous Representation

$$q_a = p_{ab} + R_{ab} \cdot q_b$$

$$\begin{bmatrix} q_a \\ 1 \end{bmatrix} = \underbrace{\begin{bmatrix} R_{ab} & p_{ab} \\ 0 & 1 \end{bmatrix}}_{\bar{g}_{ab}} \begin{bmatrix} q_b \\ 1 \end{bmatrix}$$

$$\bar{q}_a = \bar{g}_{ab} \cdot \bar{q}_b$$

□ **Composition Rule:**

$$\bar{q}_b = \bar{g}_{bc} \cdot \bar{q}_c$$

$$\bar{q}_a = \bar{g}_{ab} \cdot \bar{q}_b = \underbrace{\bar{g}_{ab} \cdot \bar{g}_{bc}}_{\bar{g}_{ac}} \cdot \bar{q}_c$$

$$\bar{g}_{ac} = \bar{g}_{ab} \cdot \bar{g}_{bc} = \begin{bmatrix} R_{ab}R_{bc} & R_{ab}p_{bc} + p_{ab} \\ 0 & 1 \end{bmatrix}$$

$$g_{ab} = (p_{ab}, R_{ab})$$



$$\bar{g}_{ab} = \begin{bmatrix} R_{ab} & p_{ab} \\ 0 & 1 \end{bmatrix}$$

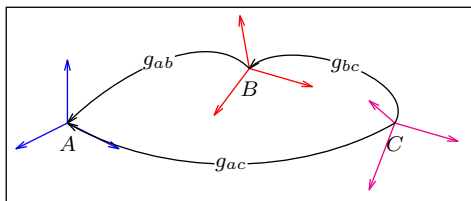


Figure 2.12

# Special Euclidean Group

$$SE(3) = \left\{ \begin{bmatrix} R & p \\ 0 & 1 \end{bmatrix} \in \mathbb{R}^{4 \times 4} \mid p \in \mathbb{R}^3, R \in SO(3) \right\}$$

**Property 4:**  $SE(3)$  forms a group.

**Proof :**

- 1  $g_1 \cdot g_2 \in SE(3)$
- 2  $e = I_4$
- 3  $(\bar{g})^{-1} = \begin{bmatrix} R^T & -R^T p \\ 0 & 1 \end{bmatrix}$
- 4 Associativity: Follows from property of matrix multiplication □

$$\bar{v} = s - r = \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ 0 \end{bmatrix}, \bar{g}_* \bar{v} = \bar{g}s - \bar{g}r = \begin{bmatrix} R & p \\ 0 & 1 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ 0 \end{bmatrix} = \begin{bmatrix} Rv \\ 0 \end{bmatrix}$$

The bar will be dropped to simplify notations

**Property 5:** An element of  $SE(3)$  is a rigid transformation.

# Exponential coordinates of $SE(3)$

**For rotational motion:**

$$\dot{p}(t) = \omega \times (p(t) - q)$$

$$\begin{bmatrix} \dot{p} \\ 0 \end{bmatrix} = \begin{bmatrix} \hat{\omega} & -\omega \times q \\ 0 & 0 \end{bmatrix} \begin{bmatrix} p \\ 1 \end{bmatrix}$$

$$\text{or } \dot{\bar{p}} = \hat{\xi} \cdot \bar{p} \Rightarrow \bar{p}(t) = e^{\hat{\xi}t} \bar{p}(0)$$

$$\text{where } e^{\hat{\xi}t} = I + \hat{\xi}t + \frac{(\hat{\xi}t)^2}{2!} + \dots$$

**For translational motion:**

$$\dot{p}(t) = v$$

$$\begin{bmatrix} \dot{p}(t) \\ 0 \end{bmatrix} = \begin{bmatrix} 0 & v \\ 0 & 0 \end{bmatrix} \begin{bmatrix} p \\ 1 \end{bmatrix}$$

$$\dot{\bar{p}}(t) = \hat{\xi} \cdot \bar{p}(t) \Rightarrow \bar{p}(t) = e^{\hat{\xi}t} \bar{p}(0)$$

$$\hat{\xi} = \begin{bmatrix} 0 & v \\ 0 & 0 \end{bmatrix}$$

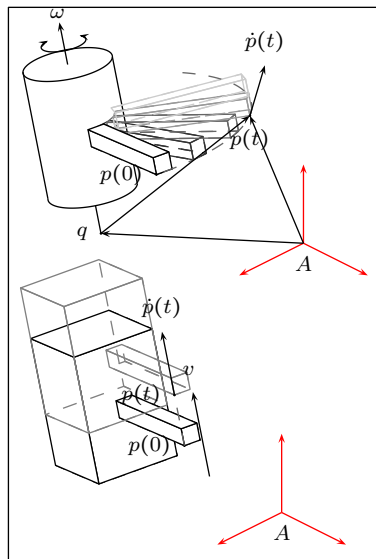


Figure 2.13



# Exponential coordinates of $SE(3)$

## Definition:

$$se(3) = \left\{ \begin{bmatrix} \hat{\omega} & v \\ 0 & 0 \end{bmatrix} \in \mathbb{R}^{4 \times 4} \mid v, \omega \in \mathbb{R}^3 \right\}$$

is called the twist space. There exists a 1-1 correspondence between  $se(3)$  and  $\mathbb{R}^6$ , defined by  $\wedge : \mathbb{R}^6 \mapsto se(3)$

$$\xi := \begin{bmatrix} v \\ \omega \end{bmatrix} \mapsto \hat{\xi} = \begin{bmatrix} \hat{\omega} & v \\ 0 & 0 \end{bmatrix}$$

**Property 6:**  $\exp : se(3) \mapsto SE(3), \hat{\xi}\theta \mapsto e^{\hat{\xi}\theta}$

## Proof :

$$\text{Let } \hat{\xi} = \begin{bmatrix} \hat{\omega} & v \\ 0 & 0 \end{bmatrix}$$

- If  $\omega = 0$ , then  $\hat{\xi}^2 = \hat{\xi}^3 = \dots = 0$ ,  $e^{\hat{\xi}\theta} = \begin{bmatrix} I & v\theta \\ 0 & 1 \end{bmatrix} \in SE(3)$

(continues next slide)



# Exponential coordinates of $SE(3)$

$$p(\theta) = e^{\hat{\xi}\theta} \cdot p(0) \Rightarrow g_{ab}(\theta) = e^{\hat{\xi}\theta}$$

If there is offset,

$$g_{ab}(\theta) = e^{\hat{\xi}\theta} g_{ab}(0) \text{ (Why?)}$$

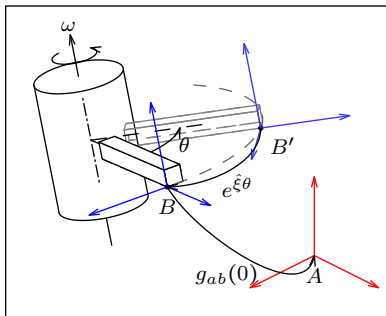


Figure 2.14

# Exponential coordinates of $SE(3)$

**Property 7:**  $\exp : se(3) \mapsto SE(3)$  is onto.

**Proof :**

Let  $g = (p, R), R \in SO(3), p \in \mathbb{R}^3$

Case 1: ( $R = I$ ) Let

$$\hat{\xi} = \begin{bmatrix} 0 & \frac{p}{\|p\|} \\ 0 & 0 \end{bmatrix}, \theta = \|p\| \Rightarrow e^{\hat{\xi}\theta} = g = \begin{bmatrix} I & p \\ 0 & 1 \end{bmatrix}$$

Case 2: ( $R \neq I$ )

$$e^{\hat{\xi}\theta} = \begin{bmatrix} e^{\hat{\omega}\theta} & (I - e^{\hat{\omega}\theta})(\omega \times v) + \omega\omega^T v\theta \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} R & p \\ 0 & 1 \end{bmatrix}$$

$$\Rightarrow \begin{cases} e^{\hat{\omega}\theta} = R \\ (I - e^{\hat{\omega}\theta})(\omega \times v) + \omega\omega^T v\theta = p \end{cases}$$

Solve for  $\omega\theta$  from previous section. Let  $A = (I - e^{\hat{\omega}\theta})\hat{\omega} + \omega\omega^T\theta, Av = p$ .

Claim:

$$A = (I - e^{\hat{\omega}\theta})\hat{\omega} + \omega\omega^T\theta := A_1 + A_2$$

$$\ker A_1 \cap \ker A_2 = \phi \Rightarrow v = A^{-1}p$$

□

$\xi\theta \in \mathbb{R}^6$ : Exponential coordinates of  $g \in SE(3)$

# Screws, twists and screw motion



## Screw attributes

Pitch:  $h = \frac{d}{\theta} (\theta = 0, h = \infty), d = h \cdot \theta$   
 Axis:  $l = \{q + \lambda\omega \mid \lambda \in \mathbb{R}\}$   
 Magnitude:  $M = \theta$

## Definition:

A **screw**  $S$  consists of an axis  $l$ , pitch  $h$ , and magnitude  $M$ . A **screw motion** is a rotation by  $\theta = M$  about  $l$ , followed by translation by  $h\theta$ , parallel to  $l$ . If  $h = \infty$ , then, translation about  $v$  by  $\theta = M$

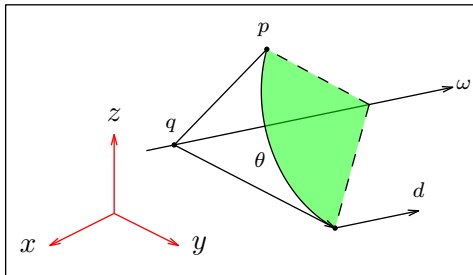


Figure 2.15

# Screws, twists and screw motion

Corresponding  $g \in SE(3)$ :

$$g \cdot p = q + e^{\hat{\omega}\theta}(p - q) + h\theta\omega$$

$$g \cdot \begin{bmatrix} p \\ 1 \end{bmatrix} = \begin{bmatrix} e^{\hat{\omega}\theta} & (I - e^{\hat{\omega}\theta})q + h\theta\omega \\ 0 & 1 \end{bmatrix} \begin{bmatrix} p \\ 1 \end{bmatrix} \Rightarrow$$

$$g = \begin{bmatrix} e^{\hat{\omega}\theta} & (I - e^{\hat{\omega}\theta})q + h\theta\omega \\ 0 & 1 \end{bmatrix}$$

On the other hand...

$$e^{\hat{\xi}\theta} = \begin{bmatrix} e^{\hat{\omega}\theta} & (I - e^{\hat{\omega}\theta})\omega \times v + \omega\omega^T v\theta \\ 0 & 1 \end{bmatrix}$$

If we let  $v = -\omega \times q + h\omega$ , then

$$(I - e^{\hat{\omega}\theta})(-\hat{\omega}^2 q) = (I - e^{\hat{\omega}\theta})(-\omega\omega^T q + q) = (I - e^{\hat{\omega}\theta})q$$

Thus,  $e^{\hat{\xi}\theta} = g$

For pure rotation ( $h = 0$ ):  $\xi = (-\omega \times q, \omega)$

For pure translation:  $g = \begin{bmatrix} I & v\theta \\ 0 & 1 \end{bmatrix}$ ,  $\Rightarrow \xi = (v, 0)$ , and  $e^{\hat{\xi}\theta} = g$



# Screw associated with a twist

Screw	Twist: $\hat{\xi}\theta$
Case 1: Pitch: $h = \infty$ Axis: $l = \{q + \lambda v \mid \ v\  = 1, \lambda \in \mathbb{R}\}$ Magnitude: $M$	$\theta = M,$ $\hat{\xi} = \begin{bmatrix} \hat{0} & v \\ 0 & 0 \end{bmatrix}$
Case 2: Pitch: $h \neq \infty$ Axis: $l = \{q + \lambda \omega \mid \ \omega\  = 1, \lambda \in \mathbb{R}\}$ Magnitude: $M$	$\theta = M,$ $\hat{\xi} = \begin{bmatrix} \hat{\omega} & -\hat{\omega}q + h\omega \\ 0 & 0 \end{bmatrix}$

## Definition: Screw Motion

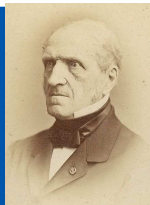
Rotation about an axis by  $\theta = M$ , followed by translation about the same axis by  $h\theta$



# Chasles Theorem

## Theorem 2 (Chasles):

Every rigid body motion can be realized by a rotation about an axis combined with a translation parallel to that axis.



1793–1880

### Proof :

For  $\hat{\xi} \in se(3)$ :

$$\hat{\xi} = \hat{\xi}_1 + \hat{\xi}_2 = \begin{bmatrix} \hat{\omega} & -\omega \times q \\ 0 & 0 \end{bmatrix} + \begin{bmatrix} 0 & h\omega \\ 0 & 0 \end{bmatrix}$$

$$[\hat{\xi}_1, \hat{\xi}_2] = 0 \Rightarrow e^{\hat{\xi}\theta} = e^{\hat{\xi}_1\theta} e^{\hat{\xi}_2\theta}$$



† End of Section †

# Velocity of a Rigid Body

## ◇ Review: Point-mass velocity

$$q(t) \in \mathbb{R}^3, t \in (-\varepsilon, \varepsilon), v = \frac{d}{dt}q(t) \in \mathbb{R}^3, a = \frac{d^2}{dt^2}q(t) = \frac{d}{dt}v(t) \in \mathbb{R}^3$$

## □ Velocity of Rotational Motion:

$$R_{ab}(t) \in SO(3), t \in (-\varepsilon, \varepsilon), q_a(t) = R_{ab}(t)q_b$$

$$V^a = \frac{d}{dt}q_a(t) = \dot{R}_{ab}(t)q_b = \dot{R}_{ab}(t)R_{ab}^T(t)R_{ab}(t)q_b = \dot{R}_{ab}R_{ab}^T q_a$$

$$R_{ab}(t)R_{ab}^T(t) = I \Rightarrow \dot{R}_{ab}R_{ab}^T + R_{ab}\dot{R}_{ab}^T = 0, \dot{R}_{ab}R_{ab}^T = -(\dot{R}_{ab}R_{ab}^T)^T$$

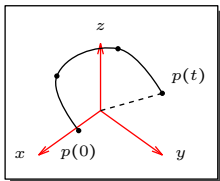


Figure 2.1

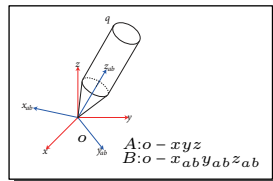


Figure 2.3

# Velocity of a Rigid Body

Denote spatial angular velocity by:

$$\hat{\omega}_{ab}^s = \dot{R}_{ab} R_{ab}^T, \omega_{ab} \in \mathbb{R}^3$$

Then

$$V^a = \hat{\omega}_{ab}^s \cdot q_a = \omega_{ab}^s \times q_a$$

Body angular velocity:

$$\hat{\omega}_{ab}^b = R_{ab}^T \cdot \dot{R}_{ab}, v^b \triangleq R_{ab}^T \cdot v^a = \omega_{ab}^b \times q_b$$

Relation between body and spatial angular velocity:

$$\omega_{ab}^b = R_{ab}^T \cdot \omega_{ab}^s \quad \text{or} \quad \hat{\omega}_{ab}^b = R_{ab}^T \hat{\omega}_{ab}^s R_{ab}$$







# Properties of Adjoint mapping

$$g^{-1} = \begin{bmatrix} R^T & -R^T p \\ 0 & 1 \end{bmatrix} \Rightarrow$$

$$\begin{aligned} \text{Ad}_{g^{-1}} &= \begin{bmatrix} R^T & (-R^T p)^\wedge R^T \\ 0 & R^T \end{bmatrix} \\ &= \begin{bmatrix} R^T & -R^T \hat{p} \\ 0 & R^T \end{bmatrix} = (\text{Ad}_g)^{-1} \end{aligned}$$

$$\text{and } \text{Ad}_{g_1 \cdot g_2} = \text{Ad}_{g_1} \cdot \text{Ad}_{g_2}$$

The map  $\text{Ad} : SE(3) \mapsto GL(\mathbb{R}^6)$ ,  $\text{Ad}(g) = \text{Ad}_g$  is a group homomorphism

Matrix Rep	Vector Rep
$\hat{\xi} \in se(3)$	$\xi \in \mathbb{R}^6$
$g \cdot \hat{\xi} \cdot g^{-1} \in se(3)$	$\text{Ad}_g \xi \in \mathbb{R}^6$

# Velocity of Screw Motion

$$g_{ab}(\theta) = e^{\hat{\xi}\theta(t)} g_{ab}(0), \quad \frac{d}{dt} e^{\hat{\xi}\theta(t)} = \hat{\xi}\dot{\theta}(t) e^{\hat{\xi}\theta(t)} = \dot{\theta}(t) e^{\hat{\xi}\theta(t)} \hat{\xi}$$

$$\begin{aligned} \hat{V}_{ab}^s &= \dot{g}_{ab} \cdot g_{ab}^{-1} = (\hat{\xi}\dot{\theta} e^{\hat{\xi}\theta(t)} g_{ab}(0)) \cdot (g_{ab}^{-1}(0) e^{-\hat{\xi}\theta(t)}) \\ &= \hat{\xi}\dot{\theta} \Rightarrow V_{ab}^s = \xi\dot{\theta} \end{aligned}$$

$$\begin{aligned} \hat{V}_{ab}^b &= g_{ab}^{-1} \cdot \dot{g}_{ab} = g_{ab}^{-1}(0) e^{-\hat{\xi}\theta} \cdot e^{\hat{\xi}\theta} \hat{\xi}\dot{\theta} g_{ab}(0) \\ &= g_{ab}^{-1}(0) \hat{\xi}\dot{\theta} g_{ab}(0) = (\text{Ad}_{g_{ab}^{-1}(0)} \xi) \wedge \dot{\theta} \Rightarrow V_{ab}^b = \text{Ad}_{g_{ab}^{-1}(0)} \xi \dot{\theta} \end{aligned}$$



# Metric Property of $se(3)$

Let  $g_i(t) \in SE(3)$ ,  $i = 1, 2$ , be representations of the same motion, obtained using coordinate frame A and B. Then,

$$g_2(t) = g_0 \cdot g_1(t) \cdot g_0^{-1} \Rightarrow V_2^s = \text{Ad}_{g_0} \cdot V_1^s$$

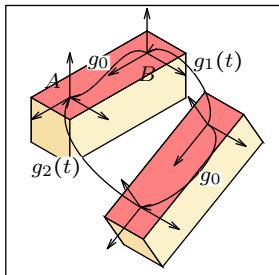


Figure 2.2

(Continues next slide)

# Metric Property of $se(3)$

$$\|V_2^s\|^2 = (\text{Ad}_{g_0} \cdot V_1^s)^T (\text{Ad}_{g_0} \cdot V_1^s) = (V_1^s)^T \text{Ad}_{g_0}^T \cdot \text{Ad}_{g_0} \cdot V_1^s$$

$$\begin{aligned} \text{Ad}_{g_0}^T \cdot \text{Ad}_{g_0} &= \begin{bmatrix} R_0^T & 0 \\ -R_0^T \hat{p}_0 & R_0^T \end{bmatrix} \begin{bmatrix} R_0 & \hat{p}_0 R_0 \\ 0 & R_0 \end{bmatrix} \\ &= \begin{bmatrix} I & R_0^T \hat{p}_0 R_0 \\ -R_0^T \hat{p}_0 R_0 & I - R_0^T \hat{p}_0^2 R_0 \end{bmatrix} \end{aligned}$$

In general,  $\|V_2^s\| \neq \|V_1^s\|$ , or there exists no bi-invariant metric on  $se(3)$ .



# Example

$$g_{ab}(\theta_1) = \begin{bmatrix} c_{\theta_1} & -s_{\theta_1} & 0 & 0 \\ s_{\theta_1} & c_{\theta_1} & 0 & 0 \\ 0 & 0 & 1 & l_0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, V_{ab}^s = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} \dot{\theta}_1$$

$$g_{bc}(\theta_2) = \begin{bmatrix} c_{\theta_2} & -s_{\theta_2} & 0 & 0 \\ s_{\theta_2} & c_{\theta_2} & 0 & l_1 \\ 0 & 0 & 1 & l_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}, V_{bc}^s = \begin{bmatrix} l_1 \\ 0 \\ 0 \\ 1 \end{bmatrix} \dot{\theta}_2$$

$$V_{ac}^s = V_{ab}^s + Ad_{g_{ab}} \cdot V_{bc}^s = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} \dot{\theta}_1 + \begin{bmatrix} l_1 c_{\theta_1} \\ l_1 s_{\theta_1} \\ 0 \\ 1 \end{bmatrix} \dot{\theta}_2$$

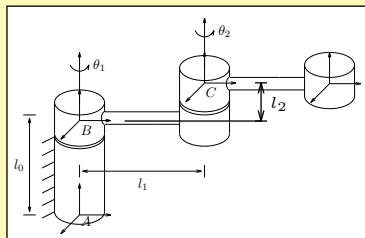


Figure 2.16

† End of Section †



## Wrenches &amp; Reciprocal Screws

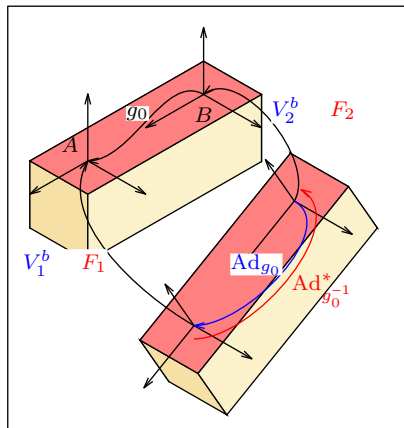


Figure 2.18

$$V_2^s = \text{Ad}_{g_0^{-1}} \cdot V_1^s$$

$$(V_2^b = \text{Ad}_{g_0^{-1}} \cdot V_1^b)$$

$$\Rightarrow V_1^b = \text{Ad}_{g_0} \cdot V_2^b$$

$$F_2 = \text{Ad}_{g_0}^* F_1$$

# Screw coordinates for a wrench

## Generate a wrench associated with $S$ :

- ( $h \neq \infty$ ): force of mag.  $M$  along  $l$ , and torque of mag.  $hM$  about  $l$ .
- ( $h = \infty$ ): pure torque of mag.  $M$  about  $l$

$$F = \begin{cases} M \begin{bmatrix} \omega \\ -\omega \times q + h\omega \end{bmatrix} & h \neq \infty \\ M \begin{bmatrix} 0 \\ \omega \end{bmatrix} & h = \infty \end{cases}$$

$F$ : wrench along the screw  $S$ .

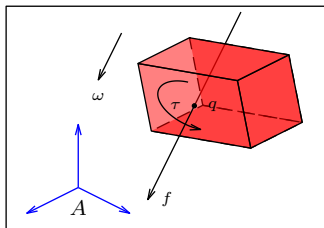


Figure 2.19

(see next page)





# Poinsot Theorem

## Theorem 3 (Poinsot):

Every collection of wrenches applied to a rigid body is equivalent to a force applied along a fixed axis plus a torque about the axis.



1777-1859

### □ Multi-fingered grasp:

$$F_O = \sum_{i=1}^k \text{Ad}_{g_{oc_i}^{-1}}^T \cdot F_{c_i}$$

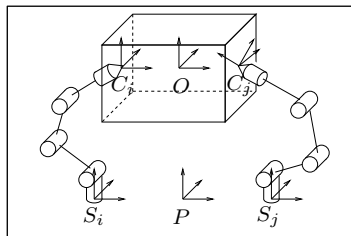


Figure 2.20



# Reciprocal screws

Given  $V = M_1 \begin{bmatrix} q_1 \times \omega_1 + h_1 \omega_1 \\ \omega_1 \end{bmatrix}$ ,  $F = M_2 \begin{bmatrix} \omega_2 \\ q_2 \times \omega_2 + h_2 \omega_2 \end{bmatrix}$ ,

Let  $q_2 = q_1 + dn$ , then

$$\begin{aligned} V \cdot F &= M_1 M_2 (\omega_2 \cdot (q_1 \times \omega_1 + h_1 \omega_1) + \omega_1 \cdot (q_2 \times \omega_2 + h_2 \omega_2)) \\ &= M_1 M_2 (\omega_2 \cdot (q_1 \times \omega_1) + h_1 \omega_1 \cdot \omega_2 \\ &\quad + \omega_1 \cdot ((q_1 + dn) \times \omega_2) + h_2 \omega_1 \cdot \omega_2) \\ &= M_1 M_2 ((h_1 + h_2) \cos \alpha - d \sin \alpha) \end{aligned}$$

# Example: basic joints

- Revolute joint:  $\xi = \begin{bmatrix} -\omega \times q \\ \omega \end{bmatrix}$

$$\xi^\perp = \text{span} \left\{ \begin{bmatrix} \omega_i \\ q \times \omega_i \end{bmatrix}, \begin{bmatrix} 0 \\ v_j \end{bmatrix} \mid \omega_i \in S^2, i = 1, 2, 3 \right\}: 5\text{-system}$$

- Prismatic joint:  $\xi = \begin{bmatrix} v \\ 0 \end{bmatrix}$

$$\xi^\perp = \text{span} \left\{ \begin{bmatrix} \omega_i \\ q \times \omega_i \end{bmatrix}, \begin{bmatrix} 0 \\ v_j \end{bmatrix} \mid \omega_i \cdot v = 0, i = 1, 2 \right. \\ \left. v_j \in S^2, j = 1, 2, 3 \right\}: 5\text{-system}$$

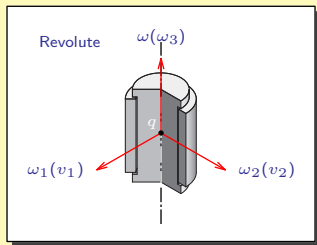


Figure 2.22

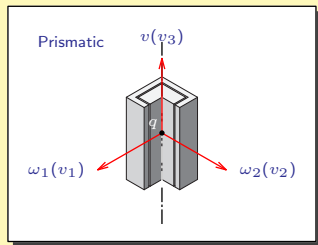


Figure 2.23



# Kinematic chains

- Universal-Spherical Dyad:

$$\xi = \text{span} \left\{ \begin{bmatrix} q_1 \times x \\ x \end{bmatrix}, \begin{bmatrix} q_1 \times y \\ y \end{bmatrix}, \begin{bmatrix} q_2 \times \omega_i \\ \omega_i \end{bmatrix} \mid \omega_i \in S^2, i = 1, 2, 3 \right\}$$

$$\xi^\perp = \text{span} \left\{ \begin{bmatrix} v \\ q_1 \times v \end{bmatrix} \mid v = \frac{q_2 - q_1}{\|q_2 - q_1\|} \right\}$$

- Revolute-Spherical Dyad: zero pitch screws passing through the center of the sphere, lie on a plane containing the axis of the revolute joint: 2-system

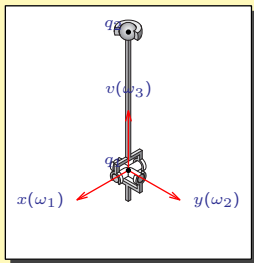


Figure 2.26

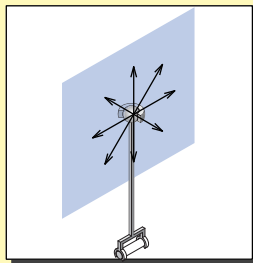


Figure 2.27 † End of Section †

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